AN-1453 LM25007 Evaluation Board

1 Introduction

The LM25007EVAL evaluation board provides the design engineer with a fully functional buck regulator, employing the constant on-time (COT) operating principle. This evaluation board provides a 5V output over an input range of 9V - 42V. The circuit delivers load currents to 450 mA, with current limit at ≅670 mA. The board is populated with all external components except C6 and C9. These components provide options for managing the output ripple as described later in this document.

The board's specification are:

- Input Voltage: 9V to 42V
- Output Voltage: 5V
- Maximum load current: 450 mA
- Minimum load current: 0 mA
- Current Limit: ≅670 mA
- Measured Efficiency: 92.6% (V_{IN} = 9V, I_{OUT} = 150 mA)
- Nominal Switching Frequency: 306 kHz
- Size: 1.6 in. x 1.0 in. x 0.5 in

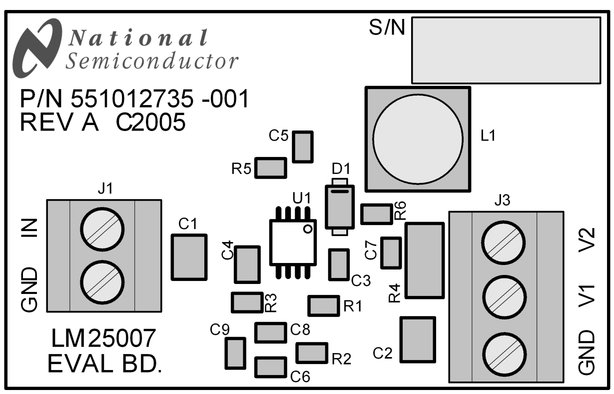

Figure 1. Evaluation Board - Top Side

2 Theory of Operation

Figure 5 contains a simplified block diagram of the LM25007. When the circuit is in regulation, the buck switch is on each cycle for a time determined by R1 and the input voltage according to Equation 1:

$$t_{ON} = \frac{1.42 \times 10^{-10} \times R1}{V_{IN}} \quad (1)$$

The nominal switching frequency is calculated from Equation 2:

$$F_S = \frac{V_{OUT}}{1.42 \times 10^{-10} \times R1} \quad (2)$$

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The on-time in this evaluation board ranges from ≅1800 ns at Vin = 9V, to ≅390 ns at Vin = 42V. The on-time varies inversely with V_{IN} to maintain a nearly constant switching frequency, which is nominally 306 kHz in this evaluation board . At the end of each on-time the Minimum Off-Timer ensures the buck switch is off for at least 300 ns. In normal operation the off-time is much longer. During the off-time the output capacitor (C2) is discharged by the load current. When the output voltage falls sufficiently that the voltage at FB is below 2.5V, the regulation comparator initiates a new on-time period. For stable, fixed frequency operation, ≅25 mVp-p of ripple is required at FB to switch the regulation comparator. For a more detailed block diagram and a complete description of the various functional blocks, see the *LM25007 42V, 0.5A Step-Down Switching Regulator Data Sheet* (SNVS401).

3 Board Layout and Probing

Figure 1 shows the placement of the circuit components. The following should be kept in mind when the board is powered:

1) When operating at high input voltage and high load current, forced air flow is recommended.

2) The LM25007 may be hot to the touch when operating at high input voltage and high load current.

3) Use CAUTION when probing the circuit at high input voltages to prevent injury, as well as possible damage to the circuit.

4) Ensure the wires connecting this board to the load are sized appropriately for the load current. Ensure there is not a significant drop in the wires between this evaluation board and the load.

4 Board Connection/Start-up

The input connections are made to the J1 connector. The load is normally connected to the V1 and GND terminals of the J3 connector. Ensure the wires are adequately sized for the intended load current. Before start-up a voltmeter should be connected to the input terminals, and to the output terminals. The load current should be monitored with an ammeter or a current probe. It is recommended that the input voltage be increased gradually to 9V, at which time the output voltage should be 5V. If the output voltage is correct with 9V at V_{IN}, then increase the input voltage as desired and proceed with evaluating the circuit.

5 Output Ripple Control

The LM25007 requires a minimum of 25 mVp-p ripple at the FB pin, in phase with the switching waveform at the SW pin, for proper operation. In the simplest configuration that ripple is derived from the ripple at V_{OUT1}, generated by the inductor's ripple current flowing through R4. That ripple voltage is attenuated by the feedback resistors, requiring that the ripple amplitude at V_{OUT1} be higher than the minimum of 25 mVp-p by the gain factor. Options for reducing the output ripple are discussed below, and the results are shown in the graph of Figure 8.

5.1 Minimum Output Ripple

This evaluation board is supplied configured for minimum ripple at V_{OUT1} by setting R4 to zero ohms, and including components R6, C7 and C8. The output ripple that ranges from 2 mVp-p at V_{IN} = 9V to 7 mVp-p at V_{IN} = 42V, is determined primarily by the ESR of output capacitor (C2), and the inductor's ripple current that ranges from 75 mAp-p to 144 mAp-p over the input voltage range. This performance applies only to continuous conduction mode as the ripple amplitude is higher in discontinuous conduction mode. The ripple voltage required by the FB pin is generated by R6, C7 and C8 since the SW pin switches from -1V to V_{IN}, and the right end of C7 is a virtual ground. The values for R6 and C7 are chosen to generate a 30-40 mVp-p triangle waveform at their junction. That triangle wave is then coupled to the FB pin through C8. The following procedure is used to calculate values for R6, C7 and C8:

- Calculate the voltage V_A:

  $$V_A = V_{OUT} - (V_{SW} \times (1 - (V_{OUT}/V_{IN}))) \quad (3)$$

  where, V_{SW} is the absolute value of the voltage at the SW pin during the off-time (typically 1V), and V_{IN} is the minimum input voltage. For this circuit V_A calculates to 4.55V. This is the DC voltage at the R6/C7 junction, and is used in Equation 4.

- Calculate the R6 x C7 product:

$$R6 \times C7 = \frac{(V_{IN} - V_A) \times t_{ON}}{\Delta V} \quad (4)$$

where, t_{ON} is the maximum on-time (≅1800 ns), V_{IN} is the minimum input voltage, and ΔV is the desired ripple amplitude at the R6/C7 junction, 30 mVp-p for this example.

$$R6 \times C7 = \frac{(9V - 4.55V) \times 1800\ ns}{0.03V} = 2.67 \times 10^{-4} \quad (5)$$

R6 and C7 are then chosen from standard value components to satisfy the above product. For example, C7 can be 2200 pF requiring R6 to be 121 kΩ. C8 is chosen to be 0.01 µF, large compared to C7. This portion of the circuit, as supplied on this EVB, is shown in Figure 2.

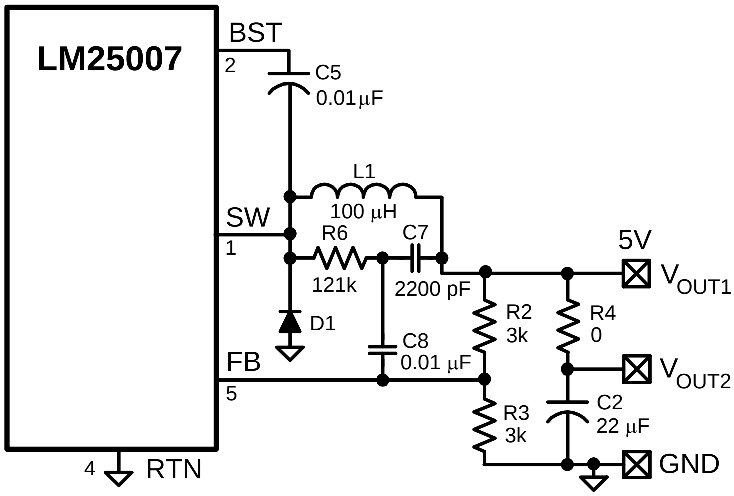

Figure 2. Minimum Ripple Using R6, C7, C8

5.2 *Intermediate Ripple Level Configuration*

This configuration generates more ripple at V_{OUT1} than the above configuration, but uses one less capacitor. If some ripple can be tolerated in the application, this configuration is slightly more economical, and simpler. R4 and C6 are used instead of R6, C7, and C8, as shown in Figure 3.

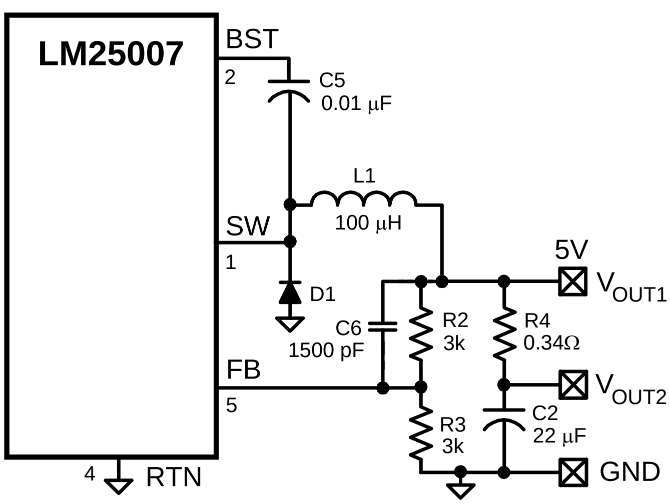

Figure 3. Intermediate Ripple Level Configuration Using C6 and R4

R4 is chosen to generate ≥25 mV at V_{OUT1}, knowing that the minimum ripple current in this circuit is 75 mAp-p at minimum V_{IN}. C6 couples that ripple to the FB pin without the attenuation of the feedback resistors. C6's minimum value is calculated from:

$$C6 = \frac{t_{ON(max)}}{(R2//R3)} \quad (6)$$

where, $t_{ON(max)}$ is the maximum on-time (at minimum V_{IN}), and R2//R3 is the equivalent parallel value of the feedback resistors. For this evaluation board $t_{ON(max)}$ is approximately 1800 ns, and R2//R3 = 1.5 kΩ, and C6 calculates to a minimum of 1200 pF. The resulting ripple at V_{OUT1} ranges from ≅25 mVp-p to 50 mVp-p over the input voltage range with the circuit in continuous conduction mode. The ripple amplitude is higher if the load current is low enough to force the circuit into discontinuous conduction mode.

5.3 Minimum Cost Configuration

This configuration is the same as Section 5.2, but without C6. Since 25 mVp-p are required at the FB pin, R4 is chosen to generate 50 mvp-p at V_{OUT1}, knowing that the minimum ripple current in this circuit is 75 mAp-p at minimum V_{IN}. To allow for tolerances, 0.68Ω is used for R4. The resulting ripple at V_{OUT1} ranges from ≅50 mVp-p to ≅100 mVp-p over the input voltage range. If the application can accept this ripple level, this is the most economical solution. The circuit is shown in Figure 4.

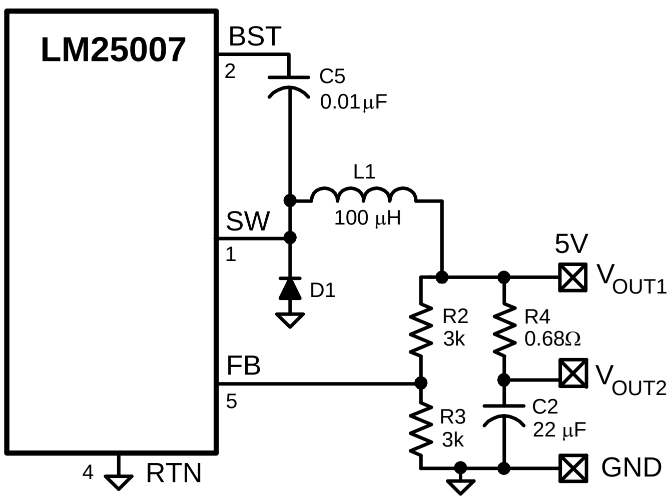

Figure 4. Minimum Cost Configuration

5.4 Alternate Low Ripple Configuration

A low ripple output can be obtained by connecting the load to V_{OUT2} in the circuits of Section 5.2 or Section 5.3. Since R4 degrades load regulation, this alternative may be viable for applications where the load current is relatively constant. If this method is used, ensure R4's power rating is appropriate for the load current.

6 Current Limit

The LM25007 contains an intelligent current limit off-timer. The current limit threshold is 725 mA, ±25%. If the current in the buck switch (the peak of the inductor's current waveform) reaches the threshold the present on-time cycle is immediately terminated, and a non-resetable off-time is initiated. The length of the off-time is controlled by an external resistor (R5) and the voltage at the FB pin. If FB = 0V (output is shorted to ground) the off-time is the preset maximum of 17 µs. This off-time ensures safe short circuit operation to the maximum input voltage of 42V. In cases of less severe overload where the output voltage, and the voltage at FB, is above ground the current limit off-time is less than 17 µs. The shorter off-times reduces the amount of foldback, recovery time, and also reduces the startup time.

The current limit off-time is calculated from Equation 7:

$$t_{OFF} = \frac{10^{-5}}{0.59 + \frac{V_{FB}}{7.22 \times 10^{-6} \times R5}} \quad (7)$$

The current limit off-time ranges from 4.3 µs to 17 µs as V_{FB} varies from 2.5V to 0V, with R5 = 200 kΩ. The guideline for selecting R5's value is that the current limit off-time (at V_{FB} = 2.5V) should be slightly longer than the maximum off-time encountered in normal operation. Setting a shorter off-time could result in inadequate overload protection, and setting a much longer off-time can affect the startup operation.

7 Minimum Load Current

The LM25007 requires a minimum load current of ≅500 µA to ensure the boost capacitor (C5) is recharged sufficiently during each off-time. In this evaluation board, the minimum load current is provided by the feedback resistors (R2, R3), allowing the board's minimum load current to be specified at zero.

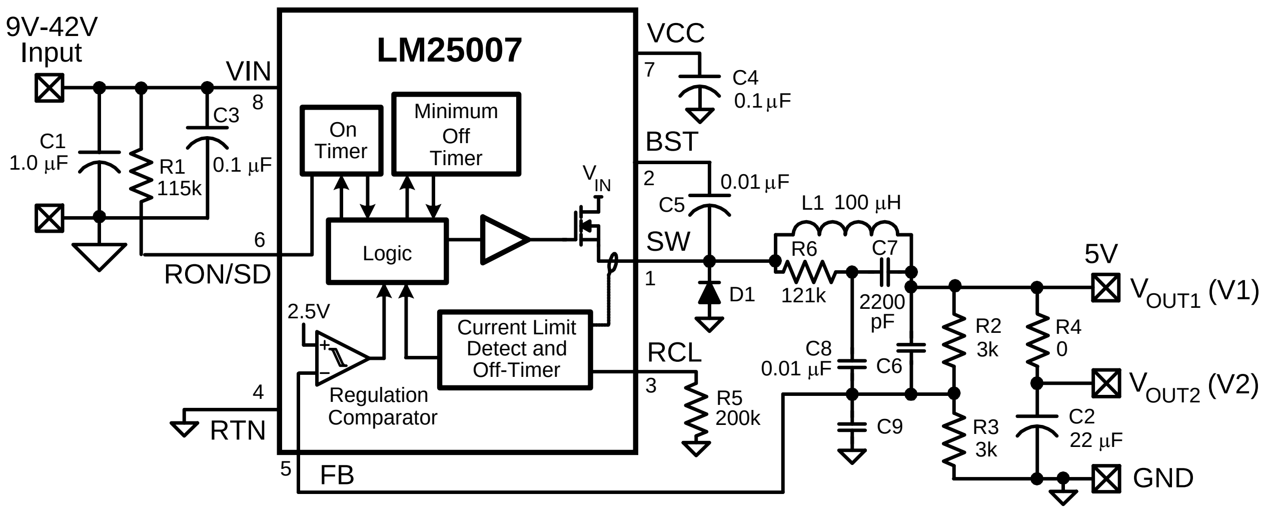

Figure 5. Complete Evaluation Board Schematic

Table 1. Bill of Materials (BOM)

Item	Description	Mfg., Part Number	Package	Value
C1	Ceramic Capacitor	TDK C3225X7R2A105M	1210	1.0 µF, 100V
C2	Ceramic Capacitor	TDK C3225X7R1C226M	1210	22 µF, 16V
C3, 4	Ceramic Capacitor	TDK C2012X7R2A104M	0805	0.1 µF, 100V
C5,8	Ceramic Capacitor	TDK C2012X7R2A103M	0805	0.01 µF, 100V
C6		Unpopulated	0805	
C7	Ceramic Capacitor	TDK C2012X7R2A222M	0805	2200 pF
C9		Unpopulated	0805	
D1	Schottky Diode	Diodes Inc. DFLS160	Power DI 123	60V, 1A
L1	Power Inductor	TDK SLF7045T-101MR50	7 mm x 7 mm	100 µH
R1	Resistor	Vishay CRCW08051153F	0805	115 kΩ
R2, 3	Resistor	Vishay CRCW08053011F	0805	3.01 kΩ
R4	Resistor	Vishay CRCW2010000Z	2010	0 Ω
R5	Resistor	Vishay CRCW08052003F	0805	200 kΩ
R6	Resistor	Vishay CRCW08051213F	0805	121 kΩ
U1	Switching Regulator	LM25007	VSSOP-8	

8 Circuit Performance

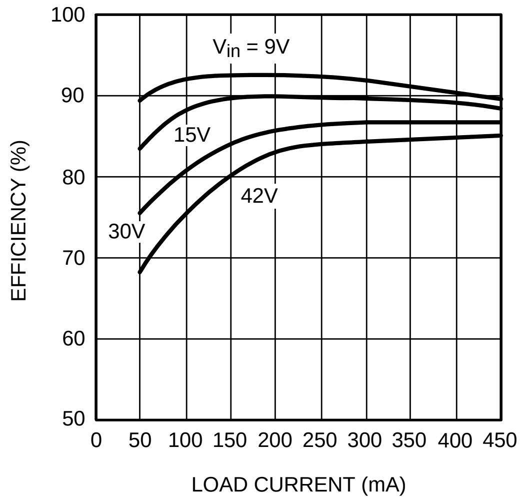

Figure 6. Efficiency vs Load Current

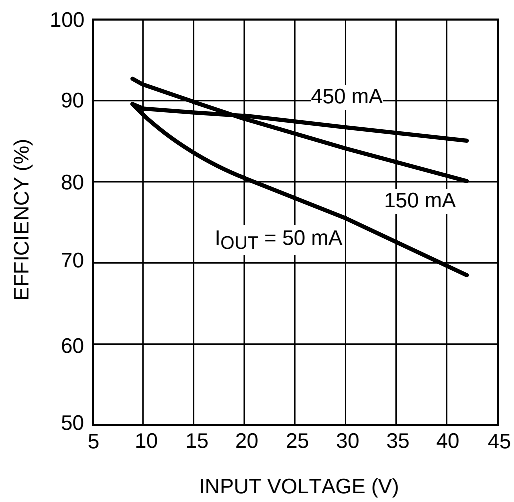

Figure 7. Efficiency vs Input Voltage

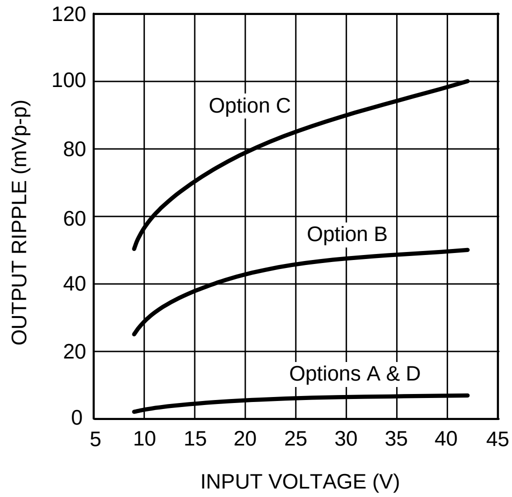

Figure 8. Output Voltage Ripple

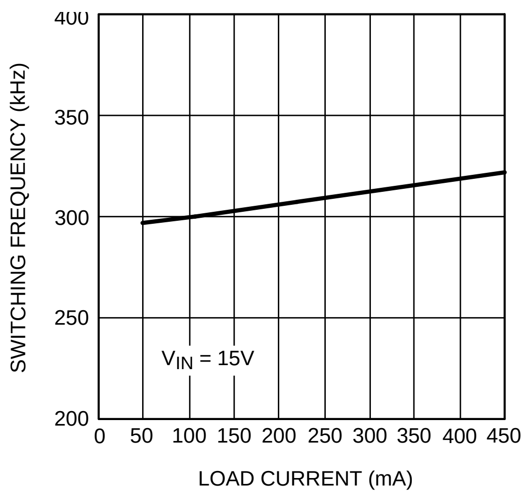

Figure 9. Switching Frequency vs. Load Current

9 PCB Layout

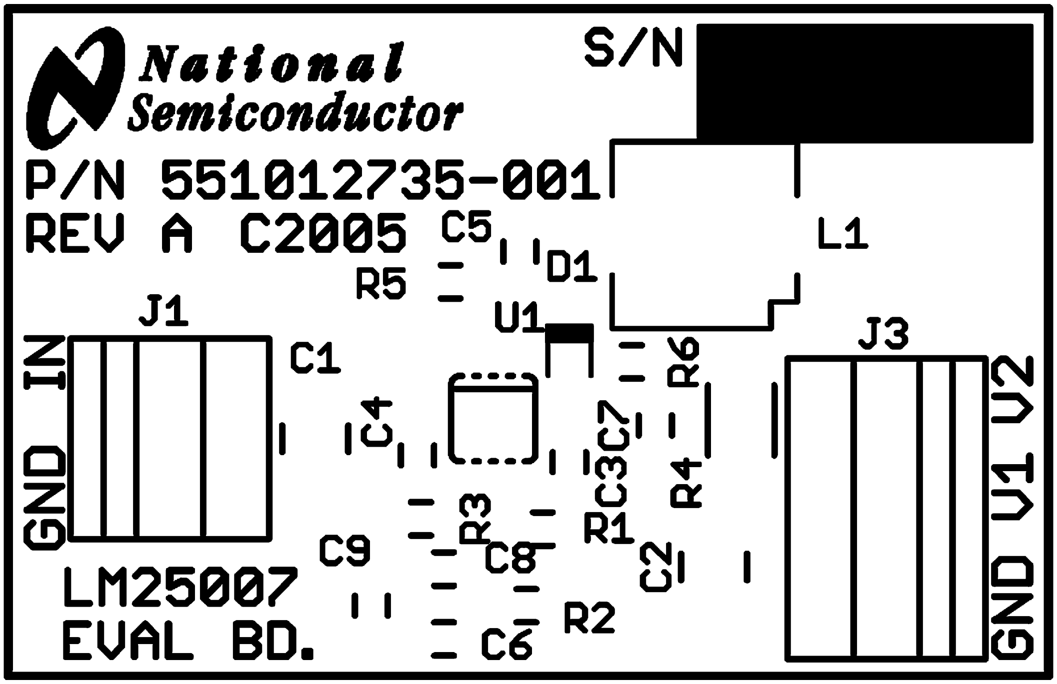

Figure 10. Board Silkscreen

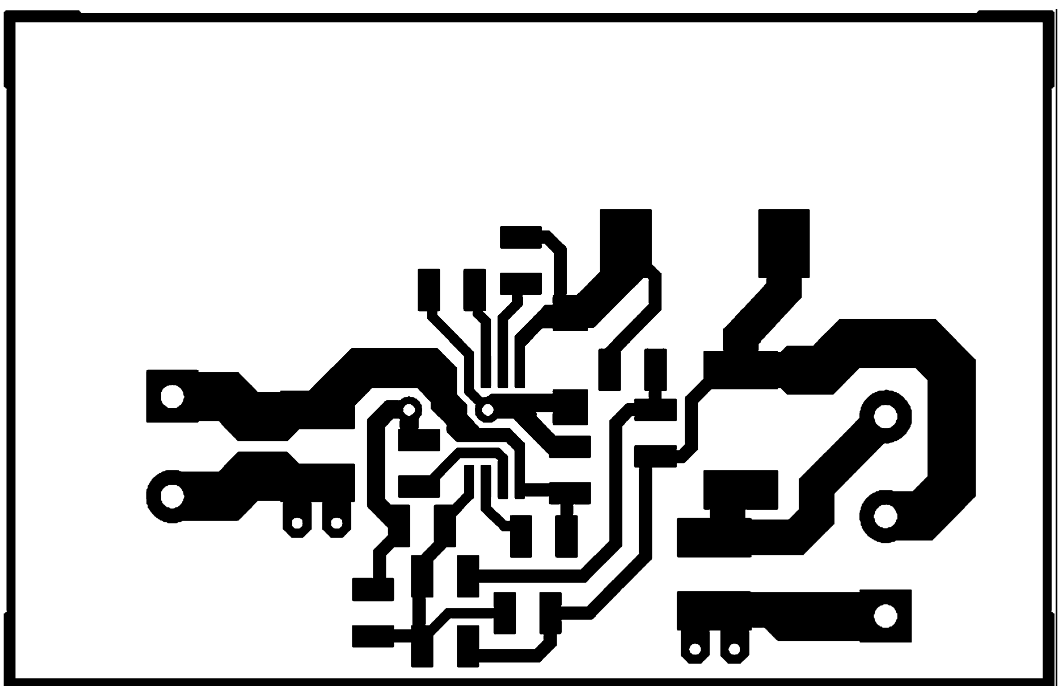

Figure 11. Board Top Layer

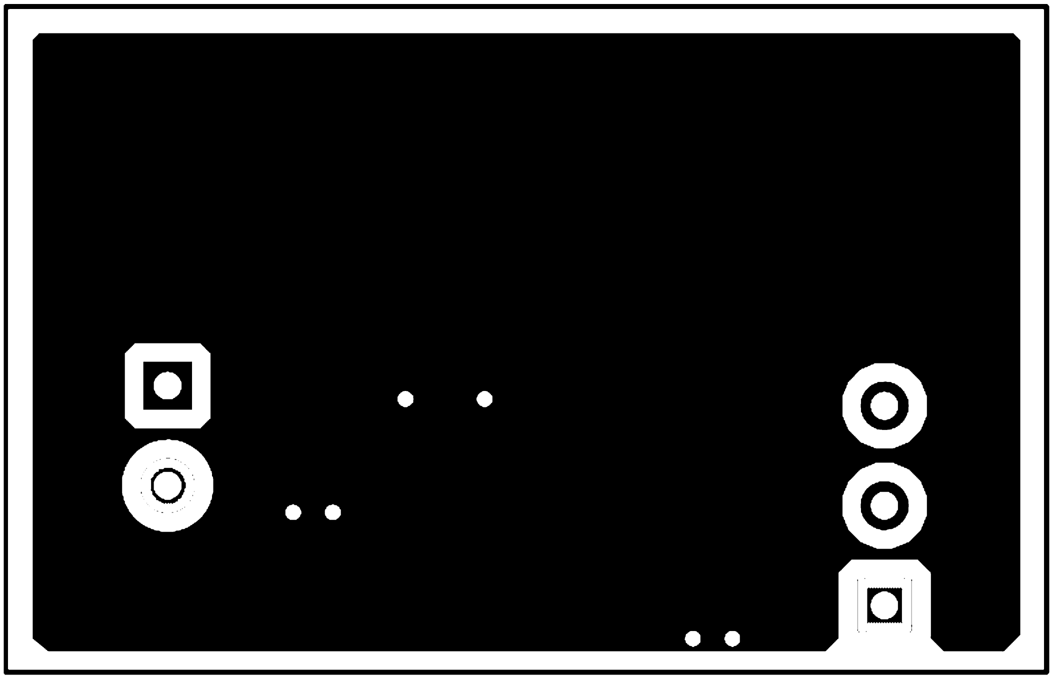

Figure 12. Board Bottom Layer (viewed from top)

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